

# Math 4997-3

## Lecture 8: Introduction to bond-based peridynamics

<https://www.cct.lsu.edu/~pdiehl/teaching/2021/4997/>

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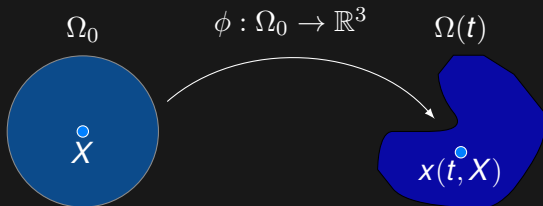
Reminder

# Lecture 8

## What you should know from last lecture

- ▶ Lambda functions
- ▶ Asynchronous programming

# Classical continuum mechanics



**Figure:** The continuum in the reference configuration  $\Omega_0$  and after the deformation  $\phi : \Omega_0 \rightarrow \mathbb{R}^3$  with  $\det(\text{grad } \phi) > 0$  in the current configuration  $\Omega(t)$  at time  $t$ .

## Prerequisites

- ▶ A material point in the continuum is identified with its position  $X \in \mathbb{R}^3$  in the so-called reference configuration  $\Omega_0 \subset \mathbb{R}^3$ .
- ▶ The reference configuration  $\Omega_0$  refers to the shape of the continuum at rest with no internal forces.

## Prerequisites

- ▶ The deformation  $\phi : [0, T] \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$  of a material point  $X$  in the reference configuration  $\Omega_0$  to the so-called current configuration  $\Omega(t)$  is given by

$$\phi(t, X) := id(X) + u(t, X) = x(t, X)$$

- ▶ where  $u : [0, T] \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$  refers to the displacement

$$u(t, X) := x(t, X) - X .$$

- ▶ The stretch  $s : [0, T] \times \mathbb{R}^3 \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$  between the material point  $X$  and the material point  $X'$  after the deformation  $\phi$  in the configuration  $\Omega(t)$  is defined by

$$s(t, X, X') := \phi(t, X') - \phi(t, X) .$$

# Notice

We just covered the prerequisites of classical continuum mechanics which are necessary to introduce the peridynamic theory. For more details, we refer to

- ▶ Liu, I-Shih. Continuum mechanics. Springer Science & Business Media, 2013.
- ▶ Gurtin, Morton E. An introduction to continuum mechanics. Vol. 158. Academic press, 1982.



# Peridynamics

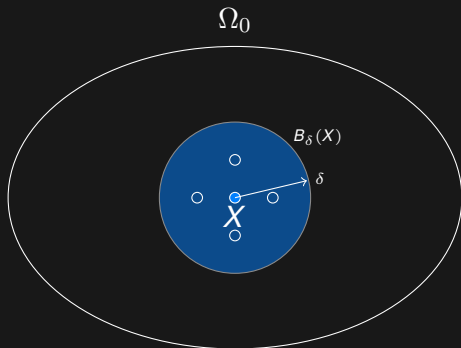
# What is peridynamics

- ▶ A non-local generalization of continuum mechanics
- ▶ Has a focus on discontinuous displacement as they arise in fracture mechanics.
- ▶ Models crack and fractures on a mesoscopic scale using Newton's second law (force equals mass times acceleration)

$$F = m \cdot a = m \cdot \ddot{X}$$

- ▶ Silling, Stewart A. "Reformulation of elasticity theory for discontinuities and long-range forces." *Journal of the Mechanics and Physics of Solids* 48.1 (2000): 175-209.
- ▶ Silling, Stewart A., and Ebrahim Askari. "A meshfree method based on the peridynamic model of solid mechanics." *Computers & structures* 83.17-18 (2005): 1526-1535.

# Principle I



**Figure:** The continuum in the reference configuration  $\Omega_0$  and the interaction zone  $B_\delta(X)$  for material point  $X$  with the horizon  $\delta$ .

# Principle II

**Acceleration**  $a : [0, T] \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$

of a material point at position  $X$  at time  $t$  is given by

$$\rho(X)a(t, X) := \int_{B_\delta(X)} f(t, \mathbf{x}(t, X') - \mathbf{x}(t, X), X' - X) dX' + b(t, X),$$

where  $f : [0, T] \times \mathbb{R}^3 \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$  denotes a pair-wise force function,  $\rho(X)$  is the mass density and  $b : [0, T] \times \mathbb{R}^3 \rightarrow \mathbb{R}^3$  the external force.

# Important fundamental assumptions

1. The medium is continuous (equal to a continuous mass density field exists)
2. Internal forces are contact forces (equal to that material points only interact if they are separated by zero distance.
3. Conservation laws of mechanics apply (conservation of mass, linear momentum, and angular momentum).

## Conservation of linear momentum

$$f(t, -(x(t, X') - x(t, X)), -(X' - X)) = -f(t, x(t, X') - x(t, X), X' - X)$$

## Conservation of angular momentum

$$(x(t, X') - x(t, X) + X' - X) \times f(t, x(t, X') - x(t, X), X' - X) = 0$$

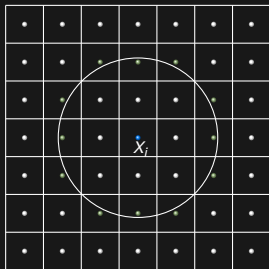
# Discretization

# EMU nodal discretization (EMU ND)

## Assumptions

- ▶ All material points  $\mathbf{X}$  are placed at the nodes  $\mathbf{X} := \{\mathbf{X}_i \in \mathbb{R}^3 | i = 1, \dots, n\}$  of a regular grid in the reference configuration  $\Omega_0$ .
- ▶ The discrete nodal spacing  $\Delta x$  between  $\mathbf{X}_i$  and  $\mathbf{X}_j$  is defined as  $\Delta x = \|\mathbf{X}_j - \mathbf{X}_i\|$ .
- ▶ The discrete interaction zone  $B_\delta(\mathbf{X}_i)$  of  $\mathbf{X}_i$  is given by  $B_\delta(\mathbf{X}_i) := \{\mathbf{X}_j | \|\mathbf{X}_j - \mathbf{X}_i\| \leq \delta\}$ .
- ▶ For all material points at the nodes  $\mathbf{X} := \{\mathbf{X}_i \in \mathbb{R}^3 | i = 1, \dots, n\}$  a surrounding volume  $\mathbf{V} := \{\mathbf{V}_i \in \mathbb{R} | i = 1, \dots, n\}$  is assumed.
- ▶ These volumes are non overlapping  $\mathbf{V}_i \cap \mathbf{V}_j = \emptyset$  and recover the volume of the volume of the reference configuration  $\sum_{i=1}^n \mathbf{V}_i = \mathbf{V}_{\Omega_0}$ .

# Discrete equation of motion



$$\rho(\mathbf{X}_i)\mathbf{a}(t, \mathbf{X}_i) = \sum_{\mathbf{X}_j \in B_\delta(\mathbf{X}_i)} \mathbf{f}(t, \mathbf{x}(t, \mathbf{X}_j) - \mathbf{x}(t, \mathbf{X}_i), \mathbf{X}_j - \mathbf{X}_i) d\mathbf{V}_j + \mathbf{b}(t, \mathbf{X}_i)$$



Note that we computed the acceleration of a material point  $a(t, X)$  and we need to compute the displacement  $u(t, X)$  by a

## Central difference scheme

$$u(t + 1, X) = 2u(t, X) - u(t - 1, X) + \Delta t^2 \left( \sum_{X_j \in B_\delta(X_i)} f(t, X_i, X_j) + b(t, X) \right)$$

to compute the actual displacement  $x(t, X) := id(X) + u(t, X)$ .

# Material models

# Prototype Microelastic Brittle (PMB) model

In this model the assumption is made that the pair-wise force  $f$  only depends on the relative normalized bond stretch  $s : [0, T] \times \mathbb{R}^3 \times \mathbb{R}^3 \rightarrow \mathbb{R}$

$$s(t, x(t, X') - x(t, X), X' - X) := \frac{\|x(t, X') - x(t, X)\| - \|X' - X\|}{\|X' - X\|}.$$

where

- ▶  $X' - X$  is the vector between the material points in the reference configuration,
- ▶  $x(t, X') - x(t, X)$  is the vector between the material point in the current configuration.

# Pair-wise bond force $f$

$$f(t, \mathbf{x}(t, \mathbf{X}') - \mathbf{x}(t, \mathbf{X}), \mathbf{X}' - \mathbf{X}) :=$$
$$c \mathbf{s}(t, \mathbf{x}(t, \mathbf{X}') - \mathbf{x}(t, \mathbf{X}), \mathbf{X}' - \mathbf{X}) \frac{\mathbf{x}(t, \mathbf{X}') - \mathbf{x}(t, \mathbf{X})}{\|\mathbf{x}(t, \mathbf{X}') - \mathbf{x}(t, \mathbf{X})\|}$$

with a material dependent stiffness constant  $c$ .

## More details:

- ▶ Silling, Stewart A., and Ebrahim Askari. "A meshfree method based on the peridynamic model of solid mechanics." *Computers & structures* 83.17-18 (2005): 1526-1535.
- ▶ Parks, Michael L., et al. "Implementing peridynamics within a molecular dynamics code." *Computer Physics Communications* 179.11 (2008): 777-783.

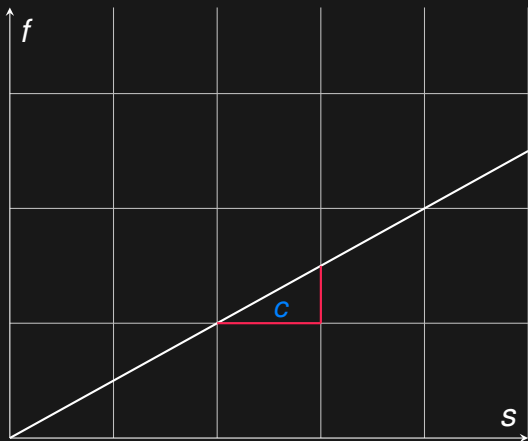


Figure: Sketch of the pair-wise linear valued force function  $f$  with the stiffness constant  $c$  as slope.

Note that there is no notion of failure/damage in the current material model.

# Introducing failure

Introduce a scalar valued history dependent function  $\mu : [0, T] \times \mathbb{R}^3 \times \mathbb{R}^3 \rightarrow \mathbb{N}$  to the computation of the pair-wise force

$$f(t, x(t, X') - x(t, X), X' - X) :=$$

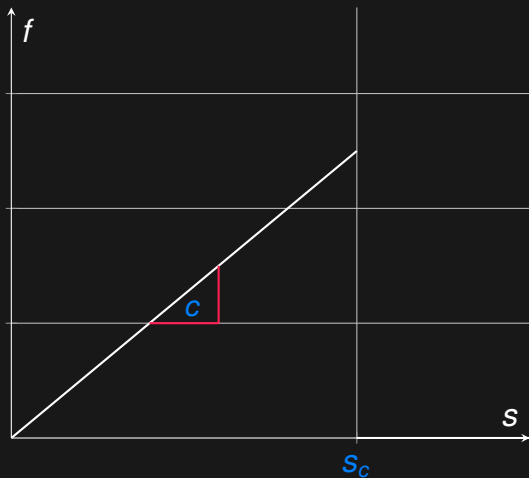
$$c s(t, x(t, X') - x(t, X), X' - X)$$

$$\mu(t, x(t, X') - x(t, X), X' - X) \frac{x(t, X') - x(t, X)}{\|x(t, X') - x(t, X)\|}.$$

with

$$\mu(t, x(t, X') - x(t, X), X' - X) := \tag{1}$$

$$\begin{cases} 1 & s(t, x(t, X') - x(t, X), X' - X) < s_c \\ 0 & \text{otherwise} \end{cases} \tag{2}$$



**Figure:** Sketch of the pair-wise linear valued force function  $f$  with the stiffness constant  $c$  as slope and the critical bond stretch  $s_c$ .

# Definition of damage

With the scalar valued history dependent function  $\mu$  the notion of damage  $d(t, X) : [0, T] \times \mathbb{R}^3 \rightarrow \mathbb{R}$  can be introduced via

$$d(t, X) := 1 - \frac{\int_{B_\delta(X)} \mu(t, x(t, X') - x(t, X), X' - X) dX'}{\int_{B_\delta(X)} dX'}.$$

To express damage in words, it is the ratio of the active (non-broken) bonds and the amount of bonds in the reference configuration within the neighborhood.



# Relation to classical continuum mechanics

## Stiffness constant

$$c = \frac{18K}{\pi\delta}$$

## Critical bond stretch

$$s_c = \sqrt{\frac{5G}{9K\delta}}$$

With

- ▶  $K$  is the bulk modulus
- ▶  $G$  is the energy release rate

# Notice

We just covered the basics of peridynamics which are necessary to implement peridynamics for the course project. For more details we refer to

- ▶ Bobaru, Florin, et al., eds. Handbook of peridynamic modeling. CRC press, 2016.
- ▶ Madenci E, Oterkus E. Peridynamic Theory. In Peridynamic Theory and Its Applications 2014 (pp. 19-43). Springer, New York, NY.

# Implementation

# Algorithm

1. Read the input files
2. Compute the neighborhoods  $B_\delta$
3. While  $t_n \leq T$ 
  - 3.1 Update the boundary conditions
  - 3.2 Compute the pair-wise forces  $f$
  - 3.3 Compute the acceleration  $a$
  - 3.4 Approximate the displacement
  - 3.5 Compute the new positions
  - 3.6 Output the simulation data
  - 3.7 Update the time step  $t_n = t_n + 1$
  - 3.8 Update the time  $t = \Delta t * t_n$

# Summary

# Summary

After this lecture, you should know

- ▶ Concept of peridynamics
- ▶ Discretization of peridynamics
- ▶ Material models

Note that this lecture is not relevant for the exams, but you should understand the content to implement the course project.

# Disclaimer

Some of the material, *e.g.* figures, plots, equations, and sentences, were adapted from P. Diehl, Modeling and Simulation of cracks and fractures with peridynamics in brittle materials, Doktorarbeit, University of Bonn, 2017.